## PLTW Engineering

PLTW Engineering Formula Sheet 2014 (v14.2)

### 1.0 Statistics

## Mean

$\mu=\frac{\sum x_{i}}{N} \quad$ (1.1a) $\quad \bar{x}=\frac{\sum x_{i}}{n}(1.1 \mathrm{~b})$
$\mu=$ population mean
$\bar{x}=$ sample mean
$\sum x_{i}=$ sum of all data values $\left(x_{1}, x_{2}, x_{3}, \ldots\right)$
$N=$ size of population
$\mathrm{n}=$ size of sample

## Median

Place data in ascending order.
If N is odd, median = central value
If N is even, median = mean of two central values
$\mathrm{N}=$ size of population

| Range (1.5) |
| :--- |
| Range $=\mathrm{x}_{\max }-\mathrm{x}_{\min }$ |
| $\mathrm{x}_{\max }=$ maximum data value |
| $\mathrm{x}_{\min }=$ minimum data value |

### 2.0 Probability

## Frequency

$\mathrm{f}_{\mathrm{x}}=\frac{\mathrm{n}_{\mathrm{x}}}{\mathrm{n}}$

## $f_{x}=$ relative frequency of outcome $x$

$\mathrm{n}_{\mathrm{x}}=$ number of events with outcome x
$\mathrm{n}=$ total number of events

## Binomial Probability (order doesn't matter)

$P_{k}=\frac{n!\left(p^{k}\right)\left(q^{n-k}\right)}{k!(n-k)!}$
$P_{k}=$ binomial probability of $k$ successes in $n$ trials
$p=$ probability of a success
$q=1-p=$ probability of failure
$k=$ number of successes
$\mathrm{n}=$ number of trials

## Mode

Place data in ascending order.
Mode $=$ most frequently occurring value
If two values occur with maximum frequency the data set is bimodal.
If three or more values occur with maximum frequency the data set is multi-modal.

## Standard Deviation

$\sigma=\sqrt{\frac{\sum\left(x_{i}-\mu\right)^{2}}{N}}$
(Population)
(1.5a)
$\mathrm{s}=\sqrt{\frac{\sum\left(\mathrm{x}_{\mathrm{i}}-\overline{\mathrm{x}}\right)^{2}}{\mathrm{n}-1}}$
(Sample)
(1.5b)
$\sigma=$ population standard deviation
$\mathrm{s}=$ sample standard deviation
$x_{i}=$ individual data value ( $x_{1}, x_{2}, x_{3}, \ldots$ )
$\mu=$ population mean
$\overline{\mathrm{x}}$ = sample mean
$\mathrm{N}=$ size of population
$\mathrm{n}=$ size of sample

## Independent Events

$\mathrm{P}(\mathrm{A}$ and B and C$)=\mathrm{P}_{\mathrm{A}} \mathrm{P}_{\mathrm{B}} \mathrm{P}_{\mathrm{C}}$
$P(A$ and $B$ and $C)=$ probability of independent
events $A$ and $B$ and $C$ occurring in sequence
$P_{A}=$ probability of event $A$

## Mutually Exclusive Events

$P(A$ or $B)=P_{A}+P_{B}$
$P(A$ or $B)=$ probability of either mutually exclusive event A or B occurring in a trial
$P_{A}=$ probability of event $A$

## Conditional Probability

$P(A \mid D)=\frac{P(A) \cdot P(D \mid A)}{P(A) \cdot P(D \mid A)+P(\sim A) \cdot P(D \mid \sim A)}$
$P(A \mid D)=$ probability of event $A$ given event $D$
$P(A)=$ probability of event $A$ occurring
$P(\sim A)=$ probability of event $A$ not occurring
$P(D \mid \sim A)=$ probability of event $D$ given event $A$ did not occur

### 3.0 Plane Geometry



## Parallelogram

Area $=b h$
(3.3)


Right Triangle


## Rectangle

Perimeter $=2 \mathrm{a}+2 \mathrm{~b}$ (3.9)
Area = ab
(3.10)


## Triangle (3.6)

Area $=1 / 2$ bh
$\mathrm{a}^{2}=\mathrm{b}^{2}+\mathrm{c}^{2}-2 \mathrm{bc} \cdot \cos \angle \mathrm{A}$
$\mathrm{b}^{2}=\mathrm{a}^{2}+\mathrm{c}^{2}-2 \mathrm{ac} \cdot \cos \angle \mathrm{B}$ $c^{2}=a^{2}+b^{2}-2 a b \cdot \cos \angle C$
(3.11)
(3.12)
(3.13)
(3.14)

Regular Polygons
Area $=\mathrm{n} \frac{\mathrm{s}\left(\frac{1}{2} \mathrm{f}\right)}{2}=\frac{\mathrm{ns}^{2}}{4 \tan \left(\frac{180}{\mathrm{n}}\right)}$

$\mathrm{n}=$ number of sides

## Trapezoid

Area $=1 / 2(a+b) h$


## Sphere

Volume $=\frac{4}{3} \pi r^{3}$
(4.8)

Surface Area $=4 \pi r^{2}$
(4.9)


## Irregular Prism

Volume $=\mathrm{Ah}$
(4.12)
$A=$ area of base

### 5.0 Constants

$g=9.8 \mathrm{~m} / \mathrm{s}^{2}=32.27 \mathrm{ft} / \mathrm{s}^{2}$
$\mathrm{G}=6.67 \times 10^{-11} \mathrm{~m}^{3} / \mathrm{kg} \cdot \mathrm{s}^{2}$
$\pi=3.14159$

### 6.0 Conversions



| Numbers Less Than One |  |  | Numbers Greater Than One |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Power of 10 | Prefix | Abbreviation | Power of 10 | Prefix | Abbreviation |
| $10^{-1}$ | deci- | d | $10^{1}$ | deca- | da |
| $10^{-2}$ | centi- | C | $10^{2}$ | hecto- | h |
| $10^{-3}$ | milli- | m | $10^{3}$ | kilo- | k |
| $10^{-6}$ | micro- | $\boldsymbol{\mu}$ | $10^{6}$ | Mega- | M |
| $10^{-9}$ | nano- | n | $10^{9}$ | Giga- | G |
| $10^{-12}$ | pico- | p | $10^{12}$ | Tera- | T |
| $10^{-15}$ | femto- | $f$ | $10^{15}$ | Peta- | P |
| $10^{-18}$ | atto- | a | $10^{18}$ | Exa- | E |
| $10^{-21}$ | zepto- | z | $10^{21}$ | Zetta- | Z |
| $10^{-24}$ | yocto- | y | $10^{24}$ | Yotta- | Y |

### 9.0 Equations

## Mass and Weight

$\begin{array}{ll}\mathrm{m}=\mathrm{VD}_{\mathrm{m}} & \text { (9.1) } \\ \mathrm{W}=\mathrm{mg} \\ \mathrm{W}=\mathrm{VD}_{\mathrm{w}} & \text { (9.2) }\end{array}$
$\mathrm{V}=$ volume
$\mathrm{D}_{\mathrm{m}}=$ mass density
$\mathrm{m}=$ mass
$\mathrm{D}_{\mathrm{w}}=$ weight density
W = weight
$\mathrm{g}=$ acceleration due to gravity

## Temperature

$\mathrm{T}_{\mathrm{K}}=\mathrm{T}_{\mathrm{C}}+273$
(9.4)
$\mathrm{T}_{\mathrm{R}}=\mathrm{T}_{\mathrm{F}}+460$
$\mathrm{T}_{\mathrm{F}}=\frac{9}{5} \mathrm{~T}_{\mathrm{c}}+32$
$\mathrm{T}_{\mathrm{K}}=$ temperature in Kelvin
$\mathrm{T}_{\mathrm{C}}=$ temperature in Celsius
$\mathrm{T}_{\mathrm{R}}=$ temperature in Rankin
$\mathrm{T}_{\mathrm{F}}=$ temperature in Fahrenheit

## Force and Moment

$\mathrm{F}=\mathrm{ma} \quad$ (9.7a) $\quad \mathrm{M}=\mathrm{Fd}_{\perp}$ (9.7b)
F = force
$\mathrm{m}=$ mass
$\mathrm{a}=$ acceleration
$\mathrm{M}=$ moment
$\mathrm{d}_{\perp}=$ perpendicular distance
Equations of Static Equilibrium
$\Sigma \mathrm{F}_{\mathrm{x}}=0 \quad \Sigma \mathrm{~F}_{\mathrm{y}}=0 \quad \Sigma \mathrm{M}_{\mathrm{P}}=0$
$\mathrm{F}_{\mathrm{x}}=$ force in the x -direction
$F_{y}=$ force in the $y$-direction
$\mathrm{M}_{\mathrm{P}}=$ moment about point P

### 9.0 Equations (Continued)

| Energy: Work |
| :--- |
| $\mathrm{W}=\mathrm{F}_{\\|} \cdot \mathrm{d}$ |
| $\mathrm{W}=$ work |
| $\mathrm{F}_{\\|}=$force parallel to direction of |
| $\quad$ displacement |
| $\mathbf{d}=$ displacement |


| Power |  |
| :--- | :--- |
| $P=\frac{E}{t}=\frac{W}{t}$ | $(9.10)$ |
| $P=\tau \omega$ | $(9.11)$ |
| $P=$ power |  |
| $E=$ energy |  |
| $W=$ work |  |
| $t=$ time |  |
| $\tau=$ torque |  |
| $\omega=$ angular velocity |  |


| Efficiency |
| :--- |
| Efficiency (\%) $=\frac{\mathrm{P}_{\text {out }}}{\mathrm{P}_{\text {in }}} \cdot 100 \% \quad(9.12)$ |
| $\mathrm{P}_{\text {out }}=$ useful power output |
| $\mathrm{P}_{\text {in }}=$ total power input |


| Energy: Potential |  |
| :--- | :--- |
| $\mathrm{U}=\mathrm{mgh}$ | $(9.13)$ |
| $\mathrm{U}=$ potential energy |  |
| $\mathrm{m}=$ mass |  |
| $\mathrm{g}=$ acceleration due to gravity |  |
| $\mathrm{h}=$ height |  |


| Energy: Kinetic |  |
| :--- | :--- |
| $\mathrm{K}=\frac{1}{2} \mathrm{mv}^{2}$ | $(9.14)$ |
| $\mathrm{K}=$ kinetic energy |  |
| $\mathrm{m}=$ mass |  |
| $\mathrm{V}=$ velocity |  |


| Energy: Thermal |
| :--- |
| $\Delta \mathrm{Q}=\mathrm{mc} \Delta \mathrm{T}$ |
| $\Delta \mathrm{Q}=$ change in thermal energy |
| $\mathrm{m}=$ mass |
| $\mathrm{c}=$ specific heat |
| $\Delta \mathrm{T}=$ change in temperature |

## Fluid Mechanics

$p=\frac{F}{A}$
$\frac{\mathrm{V}_{1}}{\mathrm{~T}_{1}}=\frac{\mathrm{V}_{2}}{\mathrm{~T}_{2}}$ (Charles' Law)
$\frac{\mathrm{p}_{1}}{\mathrm{~T}_{1}}=\frac{\mathrm{p}_{2}}{\mathrm{~T}_{2}}$ (Gay-Lussanc's Law)
$\mathrm{p}_{1} \mathrm{~V}_{1}=\mathrm{p}_{2} \mathrm{~V}_{2}$ (Boyle's Law)
$Q=A v$
$\mathrm{A}_{1} \mathrm{~V}_{1}=\mathrm{A}_{2} \mathrm{~V}_{2}$
$\mathrm{P}=\mathrm{Qp}$
absolute pressure = gauge pressure

+ atmospheric pressure (9.23)
$p=$ absolute pressure
F = force
A = area
$\mathrm{V}=$ volume
$\mathrm{T}=$ absolute temperature
$\mathrm{Q}=$ flow rate
$\mathrm{v}=$ flow velocity
$\mathrm{P}=$ power

| Mechanics |  |
| :---: | :---: |
| $\bar{s}=\frac{\mathrm{d}}{\mathrm{t}}$ | (9.24) |
| $\overline{\mathbf{v}}=\frac{\Delta \mathbf{d}}{\Delta \mathrm{t}}$ | (9.25) |
| $a=\frac{v_{f}-v_{i}}{t}$ | (9.26) |
| $X=\frac{v_{i}^{2} \sin (2 \theta)}{-g}$ | (9.27) |
| $\mathrm{v}=\mathrm{v}_{\mathrm{i}}+\mathrm{at}$ | (9.28) |
| $d=d_{i}+v_{i} t+1 / 2 a t^{2}$ | (9.29) |
| $\mathrm{v}^{2}=\mathrm{v}_{\mathrm{i}}^{2}+2 \mathrm{a}\left(\mathrm{d}-\mathrm{d}_{\mathrm{i}}\right)$ | (9.30) |
| $\boldsymbol{\tau}=\mathrm{dF} \sin \theta$ | (9.31) |
| $\overline{\mathrm{s}}$ = average speed |  |
| $\overline{\mathbf{v}}$ = average velocity |  |
| $\mathrm{v}=$ velocity |  |
| $v_{i}=$ initial velocity ( $\mathrm{t}=0$ ) |  |
| $\mathrm{a}=$ acceleration |  |
| X = range |  |
| $\mathrm{t}=$ time |  |
| $\Delta \mathbf{d}=$ change in displacement d = distance |  |
| $\mathrm{d}_{\mathrm{i}}=$ initial distance ( $\mathrm{t}=0$ ) |  |
| $\mathrm{g}=$ acceleration due to gravity |  |
| $\tau=$ torque |  |
| F = force |  |

## Electricity

Ohm's Law
$\mathrm{V}=\mathrm{IR}$
$P=I V$
$\mathrm{R}_{\mathrm{T}}$ (series) $=\mathrm{R}_{1}+\mathrm{R}_{2}+\cdots+\mathrm{R}_{\mathrm{n}}$
$\mathrm{R}_{\mathrm{T}}$ (parallel) $=\frac{1}{\frac{1}{\mathrm{R}_{1}+\frac{1}{R_{2}}+\cdots+\frac{1}{R_{n}}}}$

## Kirchhoff's Current Law

$\mathrm{I}_{\mathrm{T}}=\mathrm{I}_{1}+\mathrm{I}_{2}+\cdots+\mathrm{I}_{\mathrm{n}}$
$\quad$ or $\mathrm{I}_{\mathrm{T}}=\sum_{\mathrm{k}=1}^{\mathrm{n}} \mathrm{I}_{\mathrm{k}}$
Kirchhoff's Voltage Law

$$
\begin{align*}
& \mathrm{V}_{\mathrm{T}}=\mathrm{V}_{1}+\mathrm{V}_{2}+\cdots+\mathrm{V}_{\mathrm{n}} \\
& \quad \text { or } \quad \mathrm{V}_{\mathrm{T}}=\sum_{\mathrm{k}=1}^{\mathrm{n}} \mathrm{~V}_{\mathrm{k}} \tag{9.37}
\end{align*}
$$

$\mathrm{V}=$ voltage
$\mathrm{V}_{\mathrm{T}}=$ total voltage
I = current
$\mathrm{I}_{\mathrm{T}}=$ total current
$\mathrm{R}=$ resistance
$\mathrm{R}_{\mathrm{T}}=$ total resistance
$\mathrm{P}=$ power

## Thermodynamics

$P=Q^{\prime}=A U \Delta T$
$P=Q^{\prime}=\frac{\Delta Q}{\Delta t}$
$U=\frac{1}{R}=\frac{k}{L}$
$P=\frac{k A \Delta T}{L}$
$\mathrm{A}_{1} \mathrm{v}_{1}=\mathrm{A}_{2} \mathrm{v}_{2}$

$$
2
$$

$P_{\text {net }}=\sigma \operatorname{Ae}\left(T_{2}{ }^{4}-T_{1}{ }^{4}\right)$
$\mathrm{k}=\frac{\mathrm{PL}}{\mathrm{A} \Delta \mathrm{T}}$
$\mathrm{P}=$ rate of heat transfer
$\mathrm{Q}=$ thermal energy
$A=$ area of thermal conductivity
$U=$ coefficient of heat conductivity
(U-factor)
$\Delta T=$ change in temperature
$\Delta t=$ change in time
$R=$ resistance to heat flow ( $R$-value)
$\mathrm{k}=$ thermal conductivity
$\mathrm{v}=$ velocity
$P_{\text {net }}=$ net power radiated
$\sigma=5.6696 \times 10^{-8} \frac{\mathrm{~W}}{\mathrm{~m}^{2} \cdot \mathrm{k}^{4}}$
e = emissivity constant
$\mathrm{L}=$ thickness
$\mathrm{T}_{1}, \mathrm{~T}_{2}=$ temperature at time 1 , time 2

### 10.0 Section Properties



## Rectangle Centroid

$\bar{x}=\frac{b}{2}$ and $\bar{y}=\frac{h}{2}$
(10.3)


Right Triangle Centroid
$\bar{x}=\frac{b}{3}$ and $\bar{y}=\frac{h}{3}$
(10.4)


Semi-circle Centroid
$\bar{x}=r$ and $\bar{y}=\frac{4 r}{3 \pi}$
(10.5)

$\bar{x}=x$-distance to the centroid
$\bar{y}=y$-distance to the centroid

### 11.0 Material

| Stress (axial) |
| :--- |
| $\sigma=\frac{\mathrm{F}}{\mathrm{A}}$ |
| $\sigma=$ stress |
| $\mathrm{F}=$ axial force |
| $\mathrm{A}=$ cross-sectional area |

## Strain (axial)

$\varepsilon=\frac{\delta}{\mathrm{L}_{0}}$
$\varepsilon=$ strain
$L_{0}=$ original length
$\delta=$ change in length

## Modulus of Elasticity

$E=\frac{\sigma}{\varepsilon}$
$E=\frac{\left(F_{2}-F_{1}\right) L_{0}}{\left(\delta_{2}-\delta_{1}\right) A}$
$\mathrm{E}=$ modulus of elasticity
$\sigma=$ stress
$\varepsilon=$ strain
A = cross-sectional area
$\mathrm{F}=$ axial force
$\delta=$ deformation

| Beam Formulas |  |  |
| :---: | :---: | :---: |
|  | Reaction <br> Moment <br> Deflection | $\begin{align*} & \mathrm{R}_{\mathrm{A}}=\mathrm{R}_{\mathrm{B}}=\frac{\mathrm{P}}{2}  \tag{12.1}\\ & \mathrm{M}_{\max }=\frac{\mathrm{PL}}{4} \text { (at point of load) }  \tag{12.2}\\ & \Delta_{\max }=\frac{\mathrm{PL}^{3}}{48 \mathrm{EI}} \text { (at point of load) } \tag{12.3} \end{align*}$ |
|  | Reaction <br> Moment <br> Deflection | $\begin{align*} & R_{A}=R_{B}=\frac{\omega L}{2}  \tag{12.4}\\ & M_{\max }=\frac{\omega L^{2}}{8} \quad \text { (at center) }  \tag{12.5}\\ & \Delta_{\max }=\frac{5 \omega L^{4}}{384 E I} \quad \text { (at center) } \tag{12.6} \end{align*}$ |
|  | Reaction <br> Moment <br> Deflection | $\begin{align*} & R_{A}=R_{B}=P  \tag{12.7}\\ & M_{\max }=P a  \tag{12.8}\\ & \Delta_{\max }=\frac{P a}{24 E I}\left(3 L^{2}-4 \mathbf{a}^{2}\right)  \tag{12.9}\\ & \text { (at center) } \end{align*}$ |
|  | Reaction <br> Moment <br> Deflection | $\begin{align*} & R_{A}=\frac{P b}{L} \text { and } R_{B}=\frac{P a}{L}  \tag{12.10}\\ & M_{\max }=\frac{P a b}{L} \quad \text { (at Point of Load) (12.11) } \\ & \Delta_{\max }=\frac{\operatorname{Pab}(a+2 b) \sqrt{3 a(a+2 b)}}{27 \mathrm{EI}}  \tag{12.12}\\ & \quad \text { (at } x=\sqrt{\frac{a(a+2 b)}{3,}} \text { when } a>b \text { ) } \end{align*}$ |


| Deformation: Axial |
| :--- |
| $\delta=\frac{\mathrm{FL}_{0}}{\mathrm{AE}}$ |
| $\delta=$ deformation |
| $\mathrm{F}=$ axial force |
| $\mathrm{L}_{0}=$ original length |
| $\mathrm{A}=$ cross-sectional area |
| $\mathrm{E}=$ modulus of elasticity |

## Deformation: Axial

$\delta=\frac{\mathrm{FL}_{0}}{\mathrm{AE}}$
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## Truss Analysis

$2 \mathrm{~J}=\mathrm{M}+\mathrm{R}$
(12.14)
$\mathrm{J}=$ number of joints
M =number of members
$\mathrm{R}=$ number of reaction forces

### 13.0 Simple Machines

| Mechanical Advantage (MA) |  |  |
| :---: | :---: | :---: |
| $\mathrm{IMA}=\frac{\mathrm{D}_{\mathrm{E}}}{\mathrm{D}_{\mathrm{R}}}$ | $A M A=\frac{F_{R}}{F_{E}}$ | (13.2) |
| \% Efficiency= $\left(\frac{\text { AMA }}{\text { IMA }}\right) 100$ |  |  |
| IMA = ideal mechanical advantage |  |  |
| AMA = actual mechanical advantage |  |  |
| $\mathrm{D}_{\mathrm{E}}=$ effort distance $\mathrm{D}_{\mathrm{R}}=$ resistance distance <br> $\mathrm{F}_{\mathrm{E}}=$ effort force $\mathrm{F}_{\mathrm{R}}=$ resistance force |  |  |
|  |  |  |

Lever

## Wheel and Axle



## Pulley Systems

IMA = total number of strands of a single string supporting the resistance
(13.4)

IMA $=\frac{D_{E} \text { (string pulled) }}{D_{R}(\text { resistance lifted })}$

## Inclined Plane

$I M A=\frac{L}{H}$
(13.6)


## Wedge

$I M A=\frac{L}{H}$
(13.7)


## Screw

$I M A=\frac{C}{\text { Pitch }}$
(13.8)

Pitch $=\frac{1}{\text { TPI }}$
(13.9)


## Compound Machines

$M A_{\text {TOTAL }}=\left(M A_{1}\right)\left(M A_{2}\right)\left(M A_{3}\right) \ldots$

Gears; Sprockets with Chains; and Pulleys with Belts Ratios

$$
\begin{align*}
G R & =\frac{N_{\text {out }}}{N_{\text {in }}}=\frac{d_{\text {out }}}{d_{\text {in }}}=\frac{\omega_{\text {in }}}{\omega_{\text {out }}}=\frac{\tau_{\text {out }}}{\tau_{\text {in }}}  \tag{13.11}\\
\frac{d_{\text {out }}}{d_{\text {in }}} & \left.=\frac{\omega_{\text {in }}}{\omega_{\text {out }}}=\frac{\tau_{\text {out }}}{\tau_{\text {in }}} \text { (pulleys }\right) \tag{13.12}
\end{align*}
$$

## Compound Gears

$\mathrm{GR}_{\text {TOTAL }}=\left(\frac{\mathrm{B}}{\mathrm{A}}\right)\left(\frac{\mathrm{D}}{\mathrm{C}}\right)$

$$
\begin{aligned}
& \text { GR = gear ratio } \\
& \omega_{\text {in }}=\text { angular velocity }- \text { driver } \\
& \omega_{\text {out }}=\text { angular velocity }- \text { driven } \\
& N_{\text {in }}=\text { number of teeth }- \text { driver } \\
& N_{\text {out }}=\text { number of teeth }- \text { driven } \\
& d_{\text {in }}=\text { diameter }- \text { driver } \\
& d_{\text {out }}=\text { diameter - driven } \\
& \tau_{\text {in }}=\text { torque - driver } \\
& \tau_{\text {out }}=\text { torque - driven }
\end{aligned}
$$

### 14.0 Structural Design

## Steel Beam Design: Shear

$\mathrm{V}_{\mathrm{a}} \leq \frac{\mathrm{V}_{\mathrm{n}}}{\Omega_{\mathrm{v}}}$
$\mathrm{V}_{\mathrm{n}}=0.6 \mathrm{~F}_{\mathrm{y}} \mathrm{A}_{\mathrm{w}}$
$\mathrm{V}_{\mathrm{a}}=$ internal shear force
$\mathrm{V}_{\mathrm{n}}=$ nominal shear strength
$\Omega_{\mathrm{v}}=1.5=$ factor of safety for shear
$F_{y}=$ yield stress
$A_{w}=$ area of web
$\frac{v_{n}}{\Omega_{v}}=$ allowable shear strength

### 15.0 Storm Water Runoff

## Storm Water Drainage

$\mathrm{Q}=\mathrm{C}_{\mathrm{f}} \mathrm{CiA}$
$C_{C}=\frac{C_{1} A_{1}+C_{2} A_{2}+\cdots}{A_{1}+A_{2}+\cdots}$
$\mathrm{Q}=$ peak storm water runoff rate ( $\mathrm{ft}^{3} / \mathrm{s}$ )
$\mathrm{C}_{\mathrm{f}}=$ runoff coefficient adjustment factor
C = runoff coefficient
i = rainfall intensity (in./h)
A = drainage area (acres)

| Runoff Coefficient <br> Adjustment Factor |  |
| :--- | :--- |
| Return <br> Period | cf |
| $1,2,5,10$ | 1.0 |
| 25 | 1.1 |
| 50 | 1.2 |
| 100 | 1.25 |


| Steel Beam Design: Moment |
| :--- |
| $\mathrm{M}_{\mathrm{a}} \leq \frac{\mathrm{M}_{\mathrm{n}}}{\Omega_{\mathrm{b}}}$ |
| $\mathrm{M}_{\mathrm{n}}=\mathrm{F}_{\mathrm{y}} \mathrm{Z}_{\mathrm{x}}$ |
| $\mathrm{M}_{\mathrm{a}}=$ internal bending moment |
| $\mathrm{M}_{\mathrm{n}}=$ nominal moment strength |
| $\Omega_{\mathrm{b}}=1.67=$ factor of safety for |
| $\quad$ bending moment |
| $\mathrm{F}_{\mathrm{y}}=$ yield stress |
| $\mathrm{Z}_{\mathrm{x}}=$ plastic section modulus about |
| $\quad$ neutral axis |
| $\frac{M_{n}}{\Omega_{b}}=$ allowable bending strength |


| Rational Method Runoff Coefficients |  |
| :---: | :---: |
| Categorized by Surface |  |
| Forested | 0.059-0.2 |
| Asphalt | 0.7-0.95 |
| Brick | 0.7-0.85 |
| Concrete | 0.8-0.95 |
| Shingle roof | 0.75-0.95 |
| Lawns, well drained (sandy soil) |  |
| Up to 2\% slope | 0.05-0.1 |
| 2\% to 7\% slope | 0.10-0.15 |
| Over 7\% slope | 0.15-0.2 |
| Lawns, poor drainage (clay soil) |  |
| Up to 2\% slope | 0.13-0.17 |
| 2\% to 7\% slope | 0.18-0.22 |
| Over 7\% slope | 0.25-0.35 |
| Driveways, | 0.75-0.85 |
| Categorized by Use |  |
| Farmland | 0.05-0.3 |
| Pasture | 0.05-0.3 |
| Unimproved | 0.1-0.3 |
| Parks | 0.1-0.25 |
| Cemeteries | 0.1-0.25 |
| Railroad yard | 0.2-0.40 |
| Playgrounds | 0.2-0.35 |
| Business Districts |  |
| Neighborhood | 0.5-0.7 |
| City (downtown) | 0.7-0.95 |
| Residential |  |
| Single-family | 0.3-0.5 |
| Multi-plexes, | 0.4-0.6 |
| Multi-plexes, | 0.6-0.75 |
| Suburban | 0.25-0.4 |
| Apartments, | 0.5-0.7 |
| Industrial |  |
| Light | 0.5-0.8 |
| Heavy | 0.6-0.9 |

## Spread Footing Design

$\mathrm{q}_{\text {net }}=\mathrm{q}_{\text {allowable }}-\mathrm{p}_{\text {footing }}$
$\mathrm{p}_{\text {footing }}=\mathrm{t}_{\text {footing }} \cdot 150 \frac{\mathrm{lb}}{\mathrm{ft}^{3}}$
$q=\frac{P}{A}$
$\overline{q_{\text {net }}}=$ net allowable soil bearing pressure
$q_{\text {allowable }}=$ total allowable soil bearing pressure
$\mathrm{p}_{\text {footing }}=$ soil bearing pressure due to footing weight
$\mathrm{t}_{\text {footing }}=$ thickness of footing
$q$ = soil bearing pressure
$P=$ column load applied
A = area of footing

### 16.0 Water Supply

## Hazen-Williams Formula

$\mathrm{h}_{\mathrm{f}}=\frac{10.44 \mathrm{LQ}}{\mathrm{C}^{1.85}} \mathrm{~d}^{1.8655}$
$\mathrm{h}_{\mathrm{f}}=$ head loss due to friction (ft of $\mathrm{H}_{2} \mathrm{O}$ )
$\mathrm{L}=$ length of pipe (ft)
$\mathrm{Q}=$ water flow rate (gpm)
C = Hazen-Williams constant
d = diameter of pipe (in.)

## Dynamic Head

dynamic head = static head

- head loss (16.2)
static head = change in elevation between source and discharge


### 17.0 Heat Loss/Gain

## Heat Loss/Gain

$Q^{\prime}=A U \Delta T$
(17.1)
$U=\frac{1}{R}$
Q = thermal energy
$\mathrm{A}=$ area of thermal conductivity
$\mathrm{U}=$ coefficient of heat conductivity (U-factor)
$\Delta T=$ change in temperature
$R=$ resistance to heat flow (Rvalue)
18.0 Hazen-Williams Constants

| Pipe Material | Typical Range | Clean, New Pipe | Typical Design <br> Value |
| :---: | :---: | :---: | :---: |
| Cast Iron and <br> Wrought Iron | $80-150$ | 130 | 100 |
| Copper, Glass <br> or Brass | $120-150$ | 140 | 130 |
| Cement lined <br> Steel or Iron | 150 | 140 |  |
| Plastic <br> PVC or ABS | $120-150$ | 140 | 130 |
| Steel, welded and <br> seamless or <br> interior riveted | $80-150$ | 140 | 100 |

### 19.0 Equivalent Length of (Generic) Fittings

| Screwed Fittings |  | Pipe Size |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1/4 | 3/8 | 1/2 | 3/4 | 1 | $11 / 4$ | $11 / 2$ | 2 | $21 / 2$ | 3 | 4 |
| Elbows | Regular 90 degree | 2.3 | 3.1 | 3.6 | 4.4 | 5.2 | 6.6 | 7.4 | 8.5 | 9.3 | 11.0 | 13.0 |
|  | Long radius 90 degree | 1.5 | 2.0 | 2.2 | 2.3 | 2.7 | 3.2 | 3.4 | 3.6 | 3.6 | 4.0 | 4.6 |
|  | Regular 45 degree | 0.3 | 0.5 | 0.7 | 0.9 | 1.3 | 1.7 | 2.1 | 2.7 | 3.2 | 4.0 | 5.5 |
| Tees | Line Flow | 0.8 | 1.2 | 1.7 | 2.4 | 3.2 | 4.6 | 5.6 | 7.7 | 9.3 | 12.0 | 17.0 |
|  | Branch Flow | 2.4 | 3.5 | 4.2 | 5.3 | 6.6 | 8.7 | 9.9 | 12.0 | 13.0 | 17.0 | 21.0 |
| Return Bends | Regular 180 degree | 2.3 | 3.1 | 3.6 | 4.4 | 5.2 | 6.6 | 7.4 | 8.5 | 9.3 | 11.0 | 13.0 |
| Valves | Globe | 21.0 | 22.0 | 22.0 | 24.0 | 29.0 | 37.0 | 42.0 | 54.0 | 62.0 | 79.0 | 110.0 |
|  | Gate | 0.3 | 0.5 | 0.6 | 0.7 | 0.8 | 1.1 | 1.2 | 1.5 | 1.7 | 1.9 | 2.5 |
|  | Angle | 12.8 | 15.0 | 15.0 | 15.0 | 17.0 | 18.0 | 18.0 | 18.0 | 18.0 | 18.0 | 18.0 |
|  | Swing Check | 7.2 | 7.3 | 8.0 | 8.8 | 11.0 | 13.0 | 15.0 | 19.0 | 22.0 | 27.0 | 38.0 |
| Strainer |  |  | 4.6 | 5.0 | 6.6 | 7.7 | 18.0 | 20.0 | 27.0 | 29.0 | 34.0 | 42.0 |


| Flanged Fittings |  | Pipe Size |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1/2 | 3/4 | 1 | $11 / 4$ | $11 / 2$ | 2 | $21 / 2$ | 3 | 4 | 5 | 6 | 8 | 10 | 12 | 14 | 16 | 18 |
| Elbows | Regular 90 degree | 0.9 | 1.2 | 1.6 | 2.1 | 2.4 | 3.1 | 3.6 | 4.4 | 5.9 | 7.3 | 8.9 | 12.0 | 14.0 | 17.0 | 18.0 | 21.0 | 23.0 |
|  | Long radius 90 degree | 1.1 | 1.3 | 1.6 | 2.0 | 2.3 | 2.7 | 2.7 | 3.4 | 4.2 | 5.0 | 5.7 | 7.0 | 8.0 | 9.0 | 9.4 | 10.0 | 11.0 |
|  | Regular 45 degree | 0.5 | 0.6 | 0.8 | 1.1 | 1.3 | 1.7 | 2.0 | 2.5 | 3.5 | 4.5 | 5.6 | 7.7 | 9.0 | 11.0 | 13.0 | 15.0 | 16.0 |
| Tees | Line Flow | 0.7 | 0.8 | 1.0 | 1.3 | 1.5 | 1.8 | 1.9 | 2.2 | 2.8 | 3.3 | 3.8 | 4.7 | 5.2 | 6.0 | 6.4 | 7.2 | 7.6 |
|  | Branch Flow | 2.0 | 2.6 | 3.3 | 4.4 | 5.2 | 6.6 | 7.5 | 9.4 | 12.0 | 15.0 | 18.0 | 24.0 | 30.0 | 34.0 | 37.0 | 43.0 | 47.0 |
| Return Bends | Regular 180 degree | 0.9 | 1.2 | 1.6 | 2.1 | 2.4 | 3.1 | 3.6 | 4.4 | 5.9 | 7.3 | 8.9 | 12.0 | 14.0 | 17.0 | 18.0 | 21.0 | 23.0 |
|  | Long radius 180 degree | 1.1 | 1.3 | 1.6 | 2.0 | 2.3 | 2.7 | 2.9 | 3.4 | 4.2 | 5.0 | 5.7 | 7.0 | 8.0 | 9.0 | 9.4 | 10.0 | 11.0 |
| Valves | Globe | 38.0 | 40.0 | 45.0 | 54.0 | 59.0 | 70.0 | 77.0 | 94.0 | 120.0 | 150.0 | 190.0. | 260.0 | 310.0 | 390.0 |  |  |  |
|  | Gate |  |  |  |  |  | 2.6 | 2.7 | 2.8 | 2.9 | 3.1 | 3.2 | 3.2 | 3.2 | 3.2 | 3.2 | 3.2 | 3.2 |
|  | Angle | 15.0 | 15.0 | 17.0 | 18.0 | 18.0 | 21.0 | 22.0 | 285.0 | 38.0 | 50.0 | 63.0 | 90.0 | 120.0 | 140.0 | 160.0 | 190.0 | 210.0 |
|  | Swing Check | 3.8 | 5.3 | 7.2 | 10.0 | 12.0 | 17.0 | 21.0 | 27.0 | 38.0 | 50.0 | 63.0 | 90.0 | 120.0 | 140.0 |  |  |  |

### 20.0 555 Timer Design

$\mathrm{T}=0.693\left(\mathrm{R}_{\mathrm{A}}+2 \mathrm{R}_{\mathrm{B}}\right) \mathrm{C}$
$f=\frac{1}{\mathrm{~T}}$
duty-cycle $=\frac{\left(\mathrm{R}_{\mathrm{A}}+\mathrm{R}_{\mathrm{B}}\right)}{\left(\mathrm{R}_{\mathrm{A}}+2 \mathrm{R}_{\mathrm{B}}\right)} \cdot 100 \%$
$\mathrm{~T}=$ period
$f=$ frequency
$\mathrm{R}_{\mathrm{A}}=$ resistance A
$\mathrm{R}_{\mathrm{B}}=$ resistance B
$\mathrm{C}=$ capacitance

## 21.B Resistor Color Code

## 21.A Boolean Algebra

| Boolean Theorems |  | Consensus Theorems |  |
| :---: | :---: | :---: | :---: |
| $X \cdot 0=0$ | (21.1) | $X+\bar{X} Y=X+Y$ | (21.16) |
| $x \cdot 1=x$ | (21.2) | $X+\bar{X} \bar{Y}=X+\bar{Y}$ | (21.17) |
| $X \cdot X=X$ | (21.3) | $\bar{X}+X Y=\bar{X}+Y$ | (21.18) |
| $x \cdot \bar{X}=0$ | (21.4) | $\bar{X}+X \bar{Y}=\bar{X}+\bar{Y}$ | (21.19) |
| $x+0=X$ | (21.5) |  |  |
| $x+1=1$ | (21.6) | DeMorgan's Theorems |  |
| $X+X=X$ | (21.7) | $\overline{X Y}=\bar{X}+\bar{Y}$ | (21.20) |
| $X+\bar{X}=1$ | (21.8) | $\overline{X+Y}=\bar{X} \cdot \bar{Y}$ | (21.21) |
| $\overline{\mathrm{X}}=\mathrm{X}$ | (21.9) | Commutative Law |  |
|  |  | $X \cdot Y=Y \bullet X$ | (21.10) |
|  |  | $X+Y=Y+X$ | (21.11) |


| Associative Law |  |
| :--- | :--- |
| $\mathrm{X}(\mathrm{YZ})=(\mathrm{XY}) \mathrm{Z}$ |  |
| $\mathrm{X}+(\mathrm{Y}+\mathrm{Z})=(\mathrm{X}+\mathrm{Y})+\mathrm{Z}$ | (21.12) |

## Distributive Law

| $X(Y+Z)=X Y+X Z$ | (21.14) |
| :--- | :--- |
| $(X+Y)(W+Z)=X W+X Z+Y W+Y Z$ |  |


| Code | Tolerance |
| :---: | :---: |
| A | $\pm 0.05 \%$ |
| B | $\pm 0.1 \%$ |
| C | $\pm 0.25 \%$ |
| D | $\pm 0.5 \%$ |
| F | $\pm 1 \%$ |
| G | $\pm 2 \%$ |
| J | $\pm 5 \%$ |
| M or NONE | $\pm 20 \%$ |
| N | $\pm 30 \%$ |
| S | $-10 \%,+30 \%$ |
| T | $-20 \%,+50 \%$ |

### 23.0 G\&M Codes

| G00 $=$ Rapid Traverse | $(23.1)$ |
| :--- | :---: |
| G01 $=$ Straight Line Interpolation | $(23.2)$ |
| G02 $=$ Circular Interpolation (clockwise) | $(23.3)$ |
| G03 $=$ Circular Interpolation (c-clockwise) | $(23.4)$ |
| G04 $=$ Dwell (wait) | $(23.5)$ |
| G05 $=$ Pause for user intervention | $(23.6)$ |
| G20 $=$ Inch programming units | $(23.7)$ |
| G21 $=$ Millimeter programming units | $(23.8)$ |
| G80 $=$ Canned cycle cancel | $(23.9)$ |
| G81 $=$ Drilling cycle | $(23.10)$ |
| G82 $=$ Drilling cycle with dwell | $(23.11)$ |
| G90 $=$ Absolute Coordinates | $(23.12)$ |
| G91 $=$ Relative Coordinates | $(23.13)$ |
| M00 $=$ Pause | $(23.14)$ |
| M01 $=$ Optional stop | $(23.15)$ |
| M02 $=$ End of program | $(23.16)$ |
| M03 $=$ Spindle on | $(23.17)$ |
| M05 $=$ Spindle off | $(23.18)$ |
| M06 $=$ Tool change | $(23.19)$ |
| M08 $=$ Accessory \# 1 on | $(23.20)$ |
| M09 $=$ Accessory \# 1 off | $(23.21)$ |
| M10 $=$ Accessory \# 2 on | $(23.22)$ |
| M11 $=$ Accessory \# 2 off | $(23.23)$ |
| M30 $=$ Program end and reset | $(23.24)$ |
| M47 $=$ Rewind | $(23.25)$ |




